# **UNIVERSITI TEKNOLOGI MALAYSIA**

DECLARATION OF THESIS / UNDERGRADUATE PROJECT PAPER AND COPYRIGHT			
Author's full name : MOHD FA	IRUZ BIN OMAR		
Date of birth : 09 <sup>™</sup> FEBRL	JARY 1985		
Title : THE EFFEC BRIDGE BI	t of creep on prestressed simply supported and integral eams		
Academic Session : 2009/2010			
I declare that this thesis is classified as :			
CONFIDENTIAL	(Contains confidential information under the Official Secret Act 1972)*		
	(Contains restricted information as specified by the organization where research was done)*		
OPEN ACCESS	I agree that my thesis to be published as online open access (full text)		
I acknowledged that Universiti Teknologi Malaysia reserves the right as follows:			
<ol> <li>The thesis is the property of Universiti Teknologi Malaysia.</li> <li>The Library of Universiti Teknologi Malaysia has the right to make copies for the purpose of research only.</li> </ol>			
of research only. 3. The Library has the right to make copies of the thesis for academic exchange.			
	Certified by :		
850209-01-5205 (NEW IC NO. /PASSPORT	DR REDZUAN BIN ABDULLAH NO.) NAME OF SUPERVISOR		
Date: 20 <sup>™</sup> NOVEMBER 20	D09 Date: 20 <sup>TH</sup> NOVEMBER 2009		

**NOTES**: \* If the thesis is CONFIDENTAL or RESTRICTED, please attach with the letter from the organization with period and reasons for confidentiality or restriction.

"I hereby declare that I have read this project report and in my opinion this thesis is sufficient in terms of scope and quality for the award of the degree in Master of Engineering (Civil – Structure)"

Signature	:	
Name of Supervisor	r:	DR. REDZUAN BIN ABDULLAH
Date	:	

# THE EFFECT OF CREEP ON PRESTRESSED SIMPLY SUPPORTED AND INTEGRAL BRIDGE BEAMS

## MOHD FAIRUZ BIN OMAR

A project report submitted in partial fulfillment of the requirements for the award of the degree of Master of Engineering (Civil – Structure)

> Faculty of Civil Engineering Universiti Teknologi Malaysia

> > NOVEMBER 2009

"I declare that this project report entitled "*The Effect of Creep on Prestressed Simply Supported and Integral Bridge Beams*" is result of my own research except as cited in the references. The thesis has not been accepted for any degree and is not currently concurrently submitted in candidature of any other degree"

Signature	:	
Name	:	MOHD FAIRUZ BIN OMAR
Date	:	

Dedikasi khas buat ayah bonda dan keluarga tersayang yang sentiasa mendoakan kejayaanku siang dan malam. Terima kasih juga kepada rakan-rakan atas sokongan yang tidak berpenghujung. Moga dilindungi-Nya dunia dan akhirat.

### ACKNOWLEDGEMENT

In the name of Allah, the most compassionate and merciful. I feel very thankful to god because with His gift and guidance, the thesis can be completed on time. First of all, I would like to take this opportunity to express my sincerest appreciation to my project supervisor, Dr Redzuan Bin Abdullah for his advices and guidance throughout the course of this research. Thank you for all your support and kindness. Special thanks to Ir Mohamad Salleh Bin Yassin for being a very helpful in giving a constructive idea, supportive critics and spending a lot of time for me. A special thanks is also for my partner, Mouhammad Lutfi Bin Othman as he helped me during conducting this research. Thank you to my friends for giving idea, and sharing lots of memory along the process of finishing the thesis. Special thanks also to the people who are directly or indirectly involved in my thesis.

#### ABSTRACT

Bridge construction is one of the most important components of infrastructure development of the country. As the country develops, construction of the bridges is also increases. In Malaysia, most bridge decks are built using prestressed concrete beams supported either simply or integrally with the abutment. Under sustained compressive load due to prestressing force, the concrete beams will creep. As the result, the effective prestressing force may reduce. This thesis presents the results of a study on the effect of creep on the effective prestress force in prestressed beam. Both simply support and integral construction beams are considered. From the analysis, it is found that the integral bridge system is better than simple supported system in term of creep resistance. As indicated by vertical displacement and prestress loss, the creep is active in the prestressed beams up to 7 to 10 years for 20 to 40 meter span beams. Beyond this period, the creep gradually stops. Besides, the beam span length does not affect the amount of creep.

## ABSTRAK

Pembinaan jambatan merupakan salah satu komponen yg sangat penting dalam pembangunan infrastruktur sesebuah negara. Seiring dengan pembangunan infrastruktur ini, permintaan terhadap pembinaan jambatan juga turut meningkat. Di Malaysia, kebanyakan jambatan dibina menggunakan konkrit prategas yang dibina secata disokong mudah mahupun secara terkamir. Di bawah beban manpatan yang lama seperti daya prategas, rasuk konkrit ini akan memendek atau mengecut. Lantaran itu, daya prategas berkesan mungkin berkurangan. Tesis ini mengkaji kesan *creep* terhadap daya prategas berkesan dalam rasuk prategas. Kedua-dua jambatan jenis disokong mudah dan rasuk terkamir diambil kira. Daripada analisa yang dilakukan, didapati jambatan disokong mudah. Seperti yang ditunjukkan oleh lenturan pugak dan kehilangan prategas, fenomena *creep* hanya aktif pada 7 hingga 10 tahun pertama bagi panjang rentang 20 hingga 40 meter selepas beban dikenakan pada rasuk. Selepas itu, kesan *creep* berkurangan secara perlahan. Selain itu, perbezaan panjang rentang jambatan juga tidak mempengaruhi jumlah *creep*.

# TABLE OF CONTENT

CHAP
------

1

## CONTENT

TITLE	i			
DECLARATION	ii			
DEDICATION	iii			
ACKNOWLEDGEMENT	iv			
ABSTRACT				
ABSTRAK				
TABLE OF CONTENT	vii			
LIST OF TABLES	xi			
LIST OF FIGURES	xiii			
LIST OF APPENDICES	xvi			
INTRODUCTION	1			
1.1 Background of Study	1			
1.2 Problem Statements	2			
1.3 Research Objectives	3			
1.4 Research Questions	3			
1.5 Significant of Study	4			

2

LITERATURE REVIEW

<u>n</u>

2.1	Introdu	action	6
2.2	Integra	l Bridge Behavior	7
2.3	Creep		8
	2.3.1	Factors Influencing Creep	10
2.4	Shrink	age	11
	2.4.1	Capillary Shrinkage	11
	2.4.2	Chemical Shrinkage	13
	2.4.3	Drying Shrinkage	15
2.5	CEB-F	FIP Creep Model	16
	2.5.1	Definitions	16
	2.5.2	Range of Applicability	17
	2.5.3	Assumption and Related Basic Equations	18
	2.5.4	Creep Coefficient	19
	2.5.5	Effect of Type of Cement and Curing	20
		Temperature	
	2.5.6	Effect of High Stresses	21
2.6	Structu	aral Analysis	21
2.7	Introdu	action to Finite Element Method	22
	2.7.1	General Procedure of the FEM	22
	2.7.2	Advantages of FEM	24
2.8	Analys	sis Software: LUSAS	25

CHAP	
------	--

3

PAGE

26

# METHODOLOGY

3.1	Introdu	iction		26
3.2	Finite	Element in I	LUSAS	28
3.3	Data C	ollection		28
3.4	Modeli	ing Assump	tions	29
3.5	Model	Layout		29
	3.5.1	Longitudi	nal Beam	29
	3.5.2	Support C	onnection Detail	30
3.6	Structur	ral Modeling	g in LUSAS	32
	3.6.1	Geometry	Definition	32
	3.6.2	Attributes	Definition	33
		3.6.2.1	Meshing Attribute	33
		3.6.2.2	Geometric Attribute	35
		3.6.2.3	Material Attribute	39
		3.6.2.4	Support Attribute	40
			3.6.2.4.1 Example	42
			Calculation for Spring Stiffness	
		3.6.2.5	Loading Attribute	43
		3.6.2.6	Age, Birth and Death Attribute	44
	3.6.3	Prestress 1	Definition to BS5400	44
	3.6.4	Nonlinear	and Transient Control	46
3.7	Design	for Beam S	ection and Prestressing Force	47
	3.7.1	Prestress 1	Loss Calculation	47
3.8	Model	Verification		48
	3.8.1	Example	Calculation for Creep Coefficient,	48
		$\phi$ (t, t <sub>o</sub> )		
	3.8.2	Example	Calculation for Vertical	50
		Displaceme	ent	
3.9	Analys	is and Resu	lt Interpretation	54

CHAP		CONTENT	PAGE
4	RES	SULT AND DISCUSSION	55
	4.1	Introduction	55
	4.2	Result of Analysis	55
	4.3	Comparison of Vertical Displacement	56
	4.4	Comparison of Prestress Loss	62
	4.5	Maximum Prestress Loss	66
5	CON	NCLUSION AND RECOMMENDATION	66
	5.1	Conclusion	68
	5.2	Recommendation	69
REFER	ENC	ES	70
APPENDICES			71 - 97

# LIST OF TABLES

TABLE NO.
-----------

## TITLE

3.0	Section properties	38
3.1	Material properties	39
3.2	CEB-FIP creep material properties	40
3.3	Value of spring stiffness	43
3.4	HA loading details	43
3.5	Summary of prestressed beam properties	47
3.6	Summary of manual calculation	52
3.7	Summary of LUSAS try-and-error method	53
3.8	Comparison of LUSAS and manual calculation	53
4.1	Vertical displacement for 20 meter span obtained	56
	from LUSAS analysis	
4.2	Vertical displacement for 30 meter span obtained	58
	from LUSAS analysis	
4.3	Vertical displacement for 40 meter span obtained	60
	from LUSAS analysis	
4.4	Prestress loss due to creep for simply supported 20	62
	meter span	
4.5	Prestress loss due to creep for integral 20 meter	62
	span	
4.6	Prestress loss due to creep for simply supported 30	63
	meter span	

4.7	Prestress loss due to creep for integral 30 meter	64
	span	
4.8	Prestress loss due to creep for simply supported 40	65
	meter span	
4.9	Prestress loss due to creep for integral 40 meter	65
	span	
4.10	Maximum prestress loss due to creep within 20	66
	years	
4.11	Maximum prestress loss due to creep in percentage	67
	within 20 years	

# LIST OF FIGURES

TITLE

FIGURE NO.

		IAGE
2.0	Precast beams made integral over the interior support	7
	(O'Brien E. J., 1999)	
2.1	Deck continuous over interior support and integral	7
	with abutments (O'Brien E. J., 1999)	
2.2	Deck integral with abutments and pier (O'Brien E. J.,	7
	1999)	
2.3	Restraint against upward movement, positive	8
	secondary moment (O'Brien E. J., 1999)	
2.4	Capillary pressure and capillary shrinkage of concrete	11
	as a function of time (Bažant and Wittmann, 1982)	
2.5	Capillary shrinkage and capillary pressure of concrete	13
	as a function of time (Bažant and Wittmann, 1982)	
2.6	Swelling of the xerogel in hardened cement paste as a	16
	function of relative water vapour pressure (Bažant	
	and Wittmann, 1982)	
3.1	Research methodology flow chart	27
3.2	Longitudinal integral beam	29
3.3	Longitudinal simply supported beam	30
3.4	Integral beam-to abutment connection (Connal J.,	30
	2003)	
3.5	Integral beam-to abutment connection detail (Connal	31

# FIGURE NO.

# TITLE

J., 2003)	
-----------	--

	J., 2005)	
3.6	Simply supported beam-to abutment connection detail	31
3.7	Geometry of simply supported beam and tendon	32
3.8	Geometry of integral beam and abutments	33
3.9	Line mesh for the beam	34
3.10	Section geometry for 20 meter span	35
3.11	Section geometry for 30 meter	36
3.12	Section geometry for 40 meter	37
3.13	Section geometry for abutment	37
3.14	Pinned support	41
3.15	Roller support	41
3.16	Spring support	41
3.17	Prestress definition dialog box	45
3.18	Example of assigned prestress definition	45
3.19	Nonlinear and transient control	46
3.20	Longitudinal section of 20 meter span	50
4.1	Graph of vertical displacement against age for 20 meter	57
	simply supported prestressed beam obtained from	
	LUSAS analysis	
4.2	Graph of vertical displacement against age for 20 meter	57
	integral prestressed beam obtained from LUSAS	
	analysis	
4.3	Graph of vertical displacement against age for 30 meter	59
	simply supported prestressed beam obtained from	
	LUSAS analysis	
4.4	Graph of vertical displacement against age for 30 meter	59
	integral prestressed beam obtained from LUSAS	
	analysis	
4.5	Graph of vertical displacement against age for 40 meter	61
	simply supported prestressed beam obtained from	
	LUSAS analysis	

4.6	Graph of vertical displacement against age for 40 meter	61
	integral prestressed beam obtained from LUSAS	
	analysis	
4.7	Graph of prestress loss against years for 20 meter span	63
4.8	Graph of prestress loss against years for 30 meter span	64
4.9	Graph of prestress loss against years for 40 meter span	65
4.10	Graph of prestress loss against span length	67

# LIST OF APPENDICES

APPENDIC	TITLE	PAGE
NO.		
Α	Sample of CEB-FIP Model Code 1990 – Clause 2.1.6.4	69
В	Example of Design Calculation for Beam Section and	77
	Prestressing Force (30m Span)	

**CHAPTER I** 

#### INTRODUCTION

#### 1.1 Background of Study

Instead of simple span, recent bridges are designed and constructed in continuous spans and the number of such bridges design is increasing. This is because the number of joints in a bridge, corrosion caused by leaking joints can be reduced and the traveling public receives a better riding surface. In addition, a continuous system is tougher because it create redundancy in the system.

In general, integral bridge can be defined as a structure where the superstructure and substructures are continuous of integral with each other<sup>1</sup>. Conventional bridge system usually required more rehabilitation due to serviceability problems associated with the joints. Consequently, integral construction has recently received a great deal of attention and this form is likely to become more widespread in the future. Since the structure is designed to be continuous, it becomes much more difficult to predict the structural response of the system. Thus, further study on this area should be considered to ensure the design is safe and cost effective.

#### **1.2 Problem Statements**

Conventional prestressed concrete beam used for bridge deck are usually constructed by simple support at both ends. This type of construction requires the joint system to connect between two spans, from beam to pier and as well as beam to abutment. This joint system will automatically involve the maintenance work such as joint inspection and replacement of bearing pad. At the same time, the equipment for this maintenance is so expensive and need proper provision from expertise.

In addition, the present of joint will trap the rain water and this will increase the tendency of water absorption into the structure. This will induce the probability of steel corrosion to the structure. Moreover, the joint will make the travelling public feel uncomfortable riding surface since the material to seal the joint is not as smooth as the road pavement.

At the same time, shrinkage and creep are also affecting the prestress force in prestressed beam. This creep will reduce the prestress force and can lead to beam or bridge failure specifically. Proper prestress design must be carried out to ensure that the effect creep in prestress loss can be minimized to avoid any possibility.

The integral bridge or also known as jointless bridge, has achieved wide application in many countries due to its low construction and maintenance costs. Thus, with this research, the behavior of integral bridge can be understood and new model can be developed to suit the construction demand nowadays.

## **1.3** Research Objectives

The objectives of this study are:

- 1. To study the ability of integral bridge system in overcoming the prestress loss due to creep.
- 2. To determine the minimum time for creep to affect the prestress force of the beam.
- 3. To determine whether length of span will affect the amount of creep.

## 1.4 Research Questions

Based on this research, it is a hope so that the following research questions will be answered clearly:

- 1. Is it possible to use integral bridge system to overcome creep problem in bridge prestressed beam?
- 2. What is the maximum time for creep to affect the bridge structure?
- 3. Does the length of span influence the amount of creep?

#### 1.5 Significant of Study

The purpose of this model development study is to see how far this creep affecting prestress force in beam and how this creep and prestress force react in integral bridge. As we know, the phenomenon of creep is the source of many problems in design. Consequently, there is a need for the designer to predict whether the components operating in the creep range will sustain the life required of the structure.

This creep effect in structure especially in beam will cause the following;

- 1. Excessive deformation of structure.
- 2. Rupture in structure.
- 3. Unacceptable rates of latent flaws or initiated crack caused by creep.
- 4. Prestress loss due to creep.
- 5. Additional moment and axial force in members for integral structure.

With this research, new model of integral bridge can be developed with approximately accurate prediction which will give a positive respond to construction cost and also can improved the construction speed.

Through this research, the prestress loss due to creep can be determined and understand. If this behavior can be understand, all the design process for integral bridge can be easily and we can get a better design from the previous design.

#### **1.6** Scope of Study

Since the research has its own time constrain, several limitation have been made to ensure that the research can be completed within the time given. Follows are the limitations of this research;

- 1. The study is only interested in simply supported and integral bridge with prestressed beam.
- 2. The prestress loss is based in vertical displacement.
- 3. The prestressed beam is considering only single post-tension tendon.
- 4. The cross-section of beam considered is same along the span.
- 5. The model is a single span bridge.
- 6. The model is only for 20, 30 and 40 meters span.
- 7. The creep model is based on CEB-FIP Model Code 1990.
- 8. The model is developed using LUSAS 14 and all the result is based on the capability of this software.

## **CHAPTER II**

#### LITERATURE REVIEW

### 2.1 Introduction

Integral bridge can be defined as a bridge which the substructures and superstructure are continuous or integral with each other. Recently, integral construction has received a great deal of attention and this can be predicted to become much more widespread in the future. Previously, many bridges were constructed with expansion joints and bearings to separate the superstructure from substructure as well as the surrounding soil. This old method will leads to periodic rehabilitation due to serviceability problems associated with the joints and bearings. Consequently, bridge engineers have been trying to design bridges as jointless structure to minimize the cost of maintenance. In Malaysia particularly, the designers are now required to consider the use of the integral form for most bridges less than 60 m span.

There are many types of basic integral bridge. For example, Figure 2.0 shows the deck is composed of separate precast beams in each span. Previously, such deck might have had a joint over the central support. In-situ concrete is used to form a jointless span so that a more durable construction can be archived. Figure 2.1 show the deck is continuous over interior support and integral with abutments at the ends. Meanwhile, Figure 2.2 illustrates another variation of integral bridge with both abutments and the pier is homogenous.

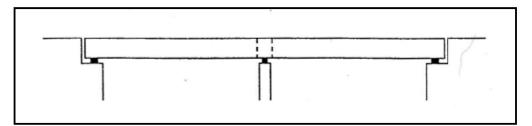


Figure 2.0: Precast beams made integral over the interior support (O'Brien E. J., 1999)

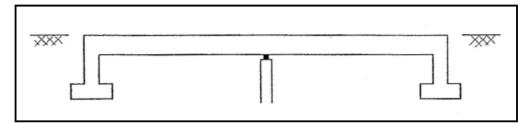


Figure 2.1: Deck continuous over interior support and integral with abutments (O'Brien E. J., 1999)

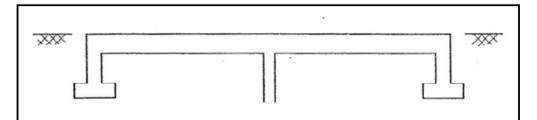


Figure 2.2: Deck integral with abutments and pier (O'Brien E. J., 1999)

#### 2.2 Integral Bridge Behavior

Since the joints and bearings are removed, their removal does affect the bridge behavior. Basically, the contraction and the expansion of the deck are restrained with the result that additional stresses are induced and must be resisted by the bridge structure. The most obvious cause of expansion and contraction in bridges of all forms is temperature change but the other causes exist, such as creep and shrinkage.

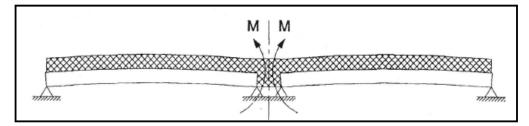


Figure 2.3: Restraint against upward movement, positive secondary moment (O'Brien E. J., 1999)

It has long been recognized that positive secondary moments developed at piers of continuous prestressed concrete bridges when the deck is cast at a relatively young beam age. In this instance, creep of the beam under the influence of prestressing predominates the response and causes an upward bow. The restraints from pier and adjacent spans result in positive secondary moments at these supports as shown in Figure 2.3. Conversely, differential shrinkage, with newer deck slab concrete shrinkage more than the beam, causes the continuous structure to bow download and result in negative secondary moments at the supports.

#### 2.3 Creep

Creep and shrinkage of concrete are complex phenomenon which is not yet understood completely. Therefore, research in this area still continues actively until recently. Based on past experimental findings on creep and shrinkage, it is believed that the origin of creep is in the microstructure of the cement paste binding the aggregate and the sand grains. The basis of this binding agent is the cement gel, which is very homogeneous material with a colloidal character. It contains chemically bonded water, colloidal water in the gel pores and free water in the capillaries and macropores. Under the effect of a long-term stress in concrete, the water, which is not bonded chemically, is extruded from the gel micropores into the capillaries, from which it evaporates. The extrusion of water is determined by the stress of concrete whereas the evaporation depends on the hygrometric conditions of the ambiance. The time-dependent deformation under sustained load due to loss of water is termed drying creep. Hence, the magnitude of creep depends on the stress in concrete, concrete mix properties and degree of hydration of concrete. It is also affected by the ambient conditions and temperature.

Wittmann F.H. (1982) claims that short-time creep is caused by a stress induced redistribution of capillary water within the structure of hardened cement paste and as well as the water movement and redistribution in the porous structure. For short-time creep we could identify one creep mechanism. For long-time creep the situation is far more complex. The xerogel forms a solid skeleton in hardened cement paste. This porous system interacts with adsorbed and capillary condensed water. In the unloaded state all gel particles are fixed to their surroundings partly by primary bonds and partly by secondary bonds. It is impossible to indicate quantitatively and in detail the bonding of an individual gel particle. But we can estimate the average coupling force.

If creep takes place the coupling force of a larger number of gel particles has to be overcome so that these particles can leave their original position in the xerogel. This movement can be looked upon as playing the role of displacement of dislocation, and vacancies in crystalline materials. Long-time creep in hardened cement paste is in fact the consequence of displacement of gel particles and to some extent creep within particles under high concentrated stress. To describe the creep process realistically we do not necessarily need to know all the different processes involved. If we know well enough the average values and if the number of particles and events is high enough we can apply rate theory. In a colloidal system such as hardened cement paste these two conditions are fulfilled. Therefore we will try to characterize the essential creep mechanisms by introducing basic elements of rate theory.

#### 2.3.1 Factors Influencing Creep

Concrete that exhibits high shrinkage generally also shows a high creep, but how the two phenomena are connected is still not understood. Evidence suggests that they are closely related. When hydrated cement is completely dried, little or no creep occurs. For a given concrete the lower the relative humidity, the higher the creep. Strength of concrete has a considerable influence on creep and within a wide range creep is inversely proportional to the strength of concrete at the time of application of load. From this it follows that creep is closely related to the water-cement ratio. There is no doubt also that the modulus of elasticity of aggregate controls the amount of creep that can be realized and concretes made with different aggregates exhibit creep of varying magnitudes.

Creep of plain concrete does not by itself affect strength, although under very high stresses creep hastens the approach of the limiting strain at which failure takes place. The influence of creep on the ultimate strength of a simply supported, reinforced concrete beam subjected to a sustained load is insignificant, but deflection increases considerably and may in many cases be a critical consideration in design. Another instance of the adverse effects of creep is its influence on the stability of the structure through increase in deformation and consequent transfer of load to other components. Thus, even when creep does not affect the ultimate strength of the component in which it takes place, its effect may be extremely serious as far as the performance of the structure as a whole is concerned.

The loss of prestress due to creep is well known and accounted for the failure of all early attempts at prestressing. Only with the introduction of high tensile steel did prestressing become a successful operation. The effects of creep may thus be harmful. On the whole, however, creep unlike shrinkage is beneficial in relieving stress concentrations and has contributed to the success of concrete as a structural material.